

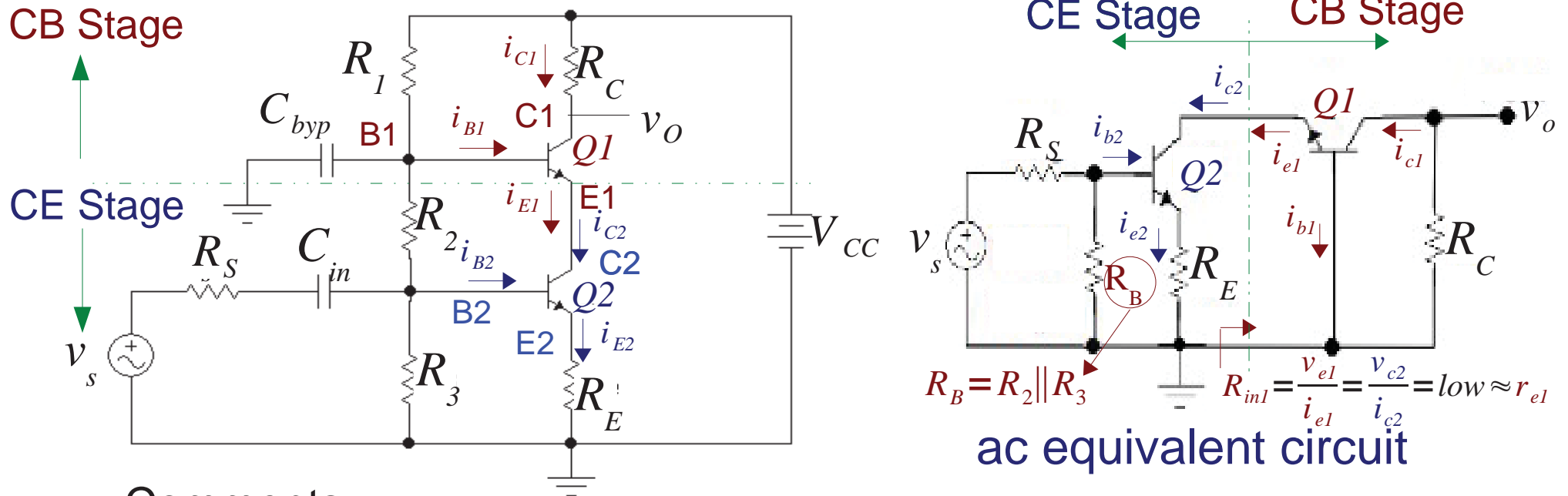
---

## *The Cascode Amplifier*

- A two transistor amplifier used to obtain simultaneously:
  1. Reasonably high input impedance.
  2. Reasonable voltage gain.
  3. Wide bandwidth.
- None of the conventional single transistor designs will satisfy all of the criteria above.
- The cascode amplifier will satisfy all of these criteria.
- A cascode is a **CE Stage** cascaded with a **CB Stage**.

**(Historical Note:** the cascode amplifier was a cascade of *grounded cathode* and *grounded grid* vacuum tube stages – hence the name “cascode,” which has remained in modern terminology.)

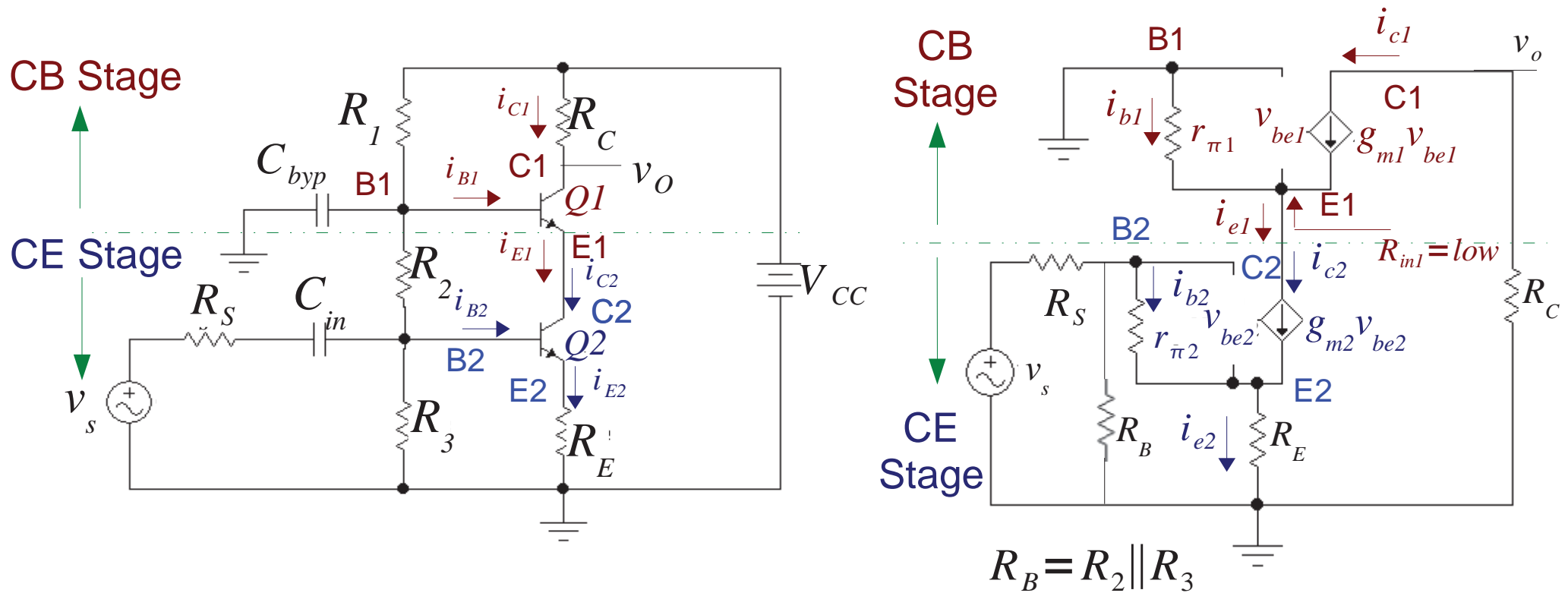
# The Cascode Amplifier



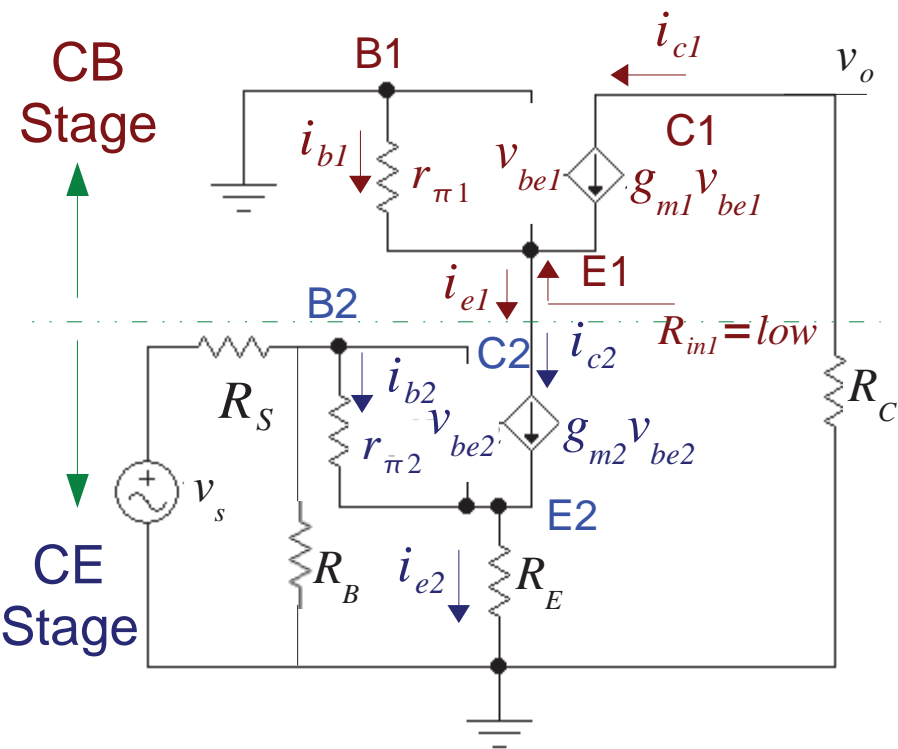
Comments:

1.  $R_1$ ,  $R_2$ ,  $R_3$ , and  $R_C$  set the bias levels for both Q1 and Q2.
2. Determine  $R_E$  for the desired voltage gain.
3.  $C_{in}$  and  $C_{byp}$  are to act as “open circuits” at dc and act as “short circuits” at all operating frequencies  $f > f_{min}$ .

# Cascode Mid-Band Small Signal Model



# Cascode Small Signal Analysis



$$g_{m1} = g_{m2} = g_m$$

$$r_{e1} = r_{e2} = r_e$$

$$r_{\pi1} = r_{\pi2} = r_{\pi}$$

1. Show reduction in Miller effect
2. Evaluate small-signal voltage gain

## OBSERVATIONS

a. The emitter current of the **CB Stage** is the collector current of the **CE Stage**. (This also holds for the dc bias current.)

$$i_{e1} = i_{c2}$$

b. The base current of the **CB Stage** is:

$$i_{b1} = \frac{i_{e1}}{\beta + 1} = \frac{i_{c2}}{\beta + 1}$$

c. Hence, both stages have about same collector current  $i_{c1} \approx i_{c2}$  and same  $g_m, r_e, r_{\pi}$ .

## Cascode Small Signal Analysis cont.

The input resistance  $R_{in1}$  to the CB Stage is the small-signal " $r_{e1}$ " for the CB Stage, i.e.

$$i_{b1} = \frac{i_{e1}}{\beta + 1} = \frac{i_{c2}}{\beta + 1}$$

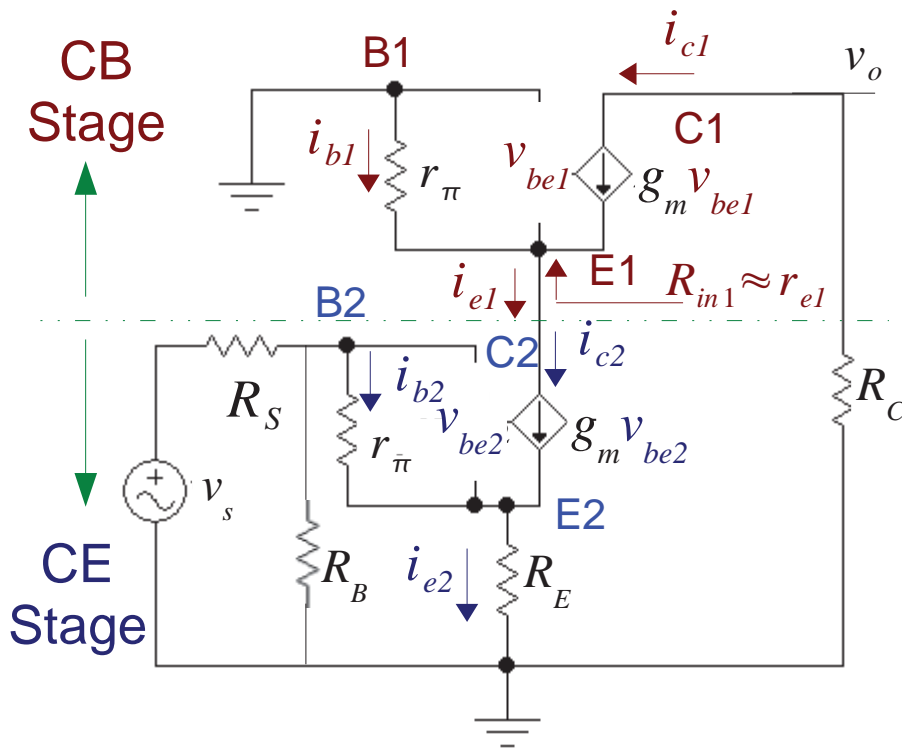
The CE output voltage, the voltage drop from Q2 collector to ground, is:

$$v_{c2} = v_{e1} = -r_{\pi} i_{b1} = -\frac{r_{\pi}}{\beta + 1} i_{c2} = -\frac{r_{\pi}}{\beta + 1} i_{e1}$$

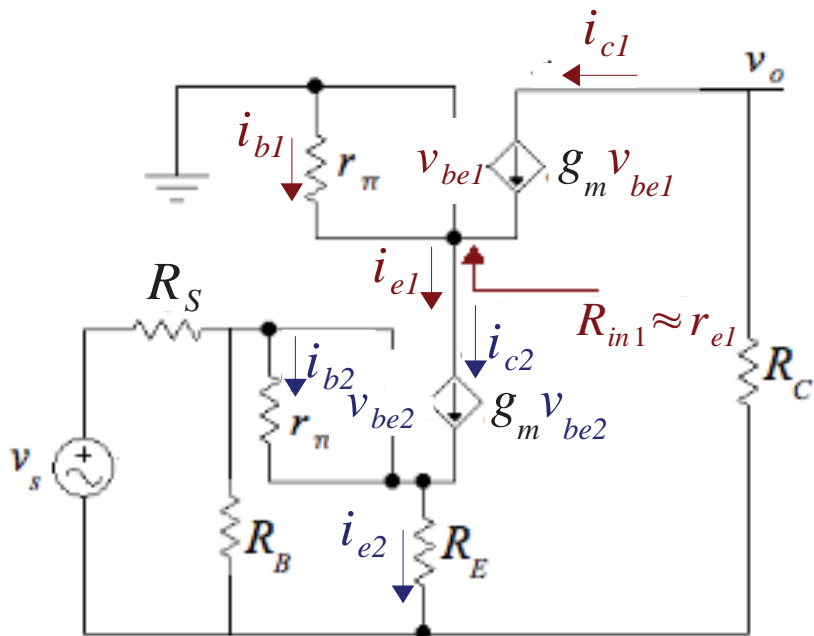
herefore, the CB Stage input resistance is:

$$R_{in1} = \frac{v_{e1}}{-i_{e1}} = \frac{r_{\pi}}{\beta + 1} = r_{e1}$$

$$A_{vCE-Stage} = \frac{v_{c2}}{v_s} \approx -\frac{R_{in1}}{R_E} = -\frac{r_e}{R_E} < 1 \Rightarrow C_{eq} = \left(1 + \frac{r_e}{R_E}\right) C_{\mu} < 2 C_{\mu}$$



## Cascode Small Signal Analysis - cont.



Now, find the CE collector current in terms of the input voltage  $v_s$ : Recall  $i_{c1} \approx i_{c2}$

$$i_{b2} \approx \frac{v_s}{R_S \parallel R_B + r_\pi + (\beta + 1) R_E}$$

$$i_{c2} = \beta i_{b2} \approx \frac{\beta v_s}{R_S \parallel R_B + r_\pi + (\beta + 1) R_E} \approx \frac{\beta v_s}{(\beta + 1) R_E}$$

for bias insensitivity:  $(\beta + 1) R_E \gg R_S \parallel R_B + r_\pi$

$$i_{c1} \approx i_{e1} = i_{c2} \approx i_{e2}$$

$$i_{c2} \approx \frac{v_s}{R_E}$$

$$v_o = -i_{c2} R_C$$

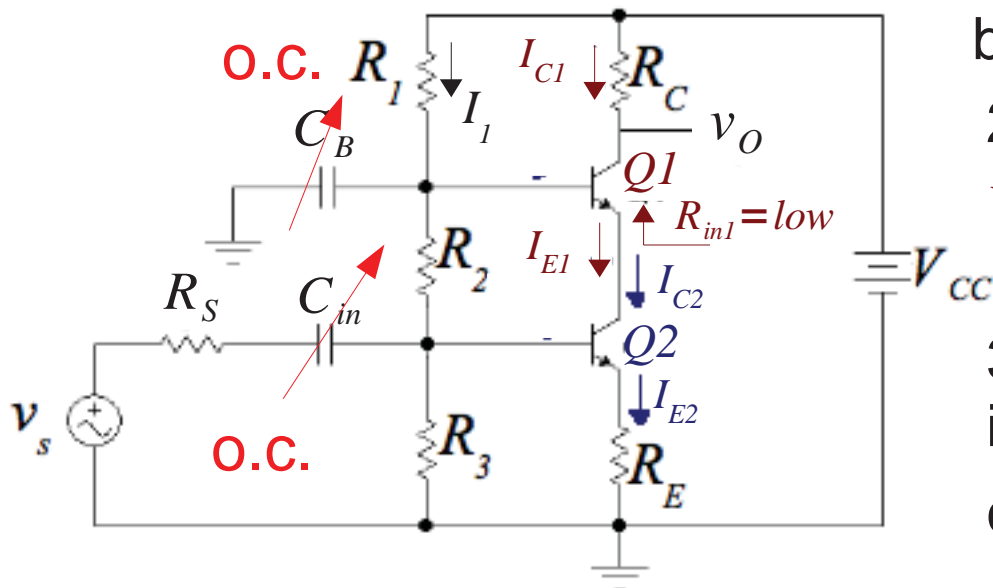
$\Rightarrow$

$$A_v = \frac{v_o}{v_s} = \frac{-R_C}{R_E}$$

**OBSERVATIONS:**

1. Voltage gain  $A_v$  is about the same as a stand-alone CE Amplifier.
2. HF cutoff is much higher than a CE Amplifier due to the reduced  $C_{eq}$ .

## Cascode Biasing



1. Choose  $I_{E1}$  – make it relatively large to reduce  $R_{in1} = r_e = V_T / I_{E1}$  to push out HF break frequencies.

2. Choose  $R_C$  for suitable voltage swing  $V_{C1}$  and  $R_E$  for desired gain.

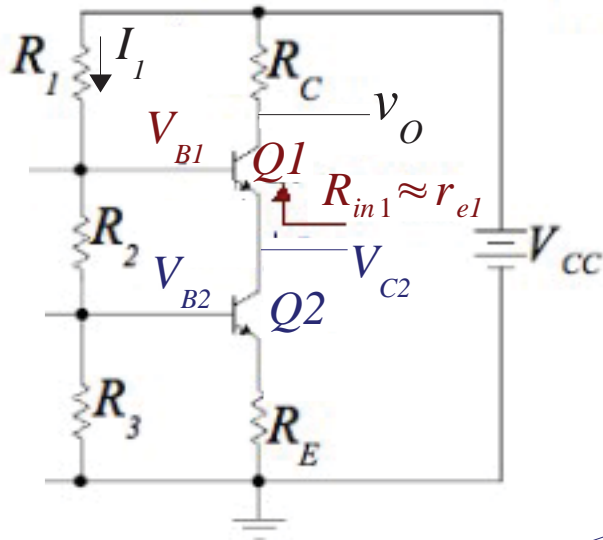
3. Choose bias resistor string such that its current  $I_1$  is about 0.1 of the collector current  $I_{C1}$ .

4. Given  $R_E$ ,  $I_{E2}$  and  $V_{BE2} = 0.7 \text{ V}$  calc.  $R_3$ .

5. Need to also determine  $R_1$  &  $R_2$ .

$$\alpha_2 I_{E2} = I_{C2} = I_{E1} = \frac{1}{\alpha_1} I_{C1} \Rightarrow I_{C1} \approx I_{E2}$$

## Cascode Biasing - cont.



Since the CE-Stage gain is very small:  
 a. The collector swing of Q2 will be small.  
 b. The Q2 collector bias  $V_{C2} = V_{B1} - 0.7 V$ .

6. Set  $V_{B1} - V_{B2} = 1 V \Rightarrow V_{CE2} = 1 V$

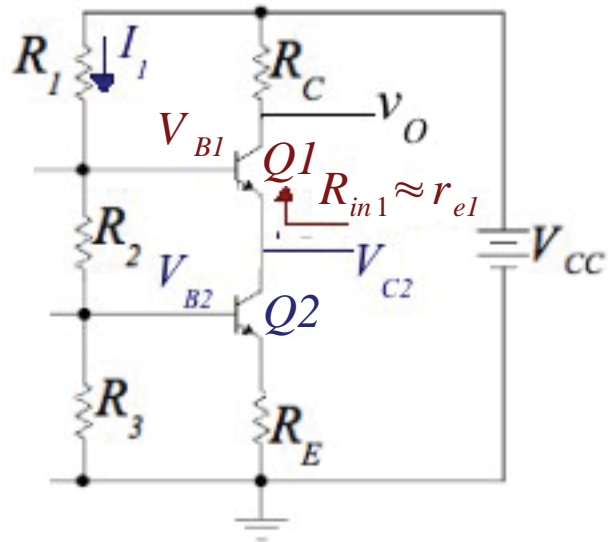
This will limit  $V_{CB2}$   $V_{CB2} = V_{CE2} - V_{BE2} = 0.3 V$   
 which will keep Q2 forward active.

$$\begin{aligned} V_{CE2} &= V_{C2} - V_{Re} = V_{C2} - (V_{B2} - 0.7 V) \\ &= V_{B1} - 0.7 V - V_{B2} + 0.7 V \\ &\therefore = V_{B1} - V_{B2} \end{aligned}$$

7. Next determine  $R_2$ . Its drop  $V_{R2} = 1 V$   
 with the known current.  $R_2 = \frac{V_{B1} - V_{B2}}{I_1}$



## Cascode Biasing - cont.



$$R_2 = \frac{V_{B1} - V_{B2}}{I_1} = \frac{1V}{I_1}$$

8. Then calculate  $R_3$ .  $R_3 = \frac{V_{B2}}{I_1}$

where  $V_{B2} = 0.7V + I_E R_E$

Note:  $R_1 + R_2 + R_3 = \frac{V_{CC}}{I_1}$

9. Then calculate  $R_1$ .

$$R_1 = \frac{V_{CC}}{0.1 I_C} - R_2 - R_3$$

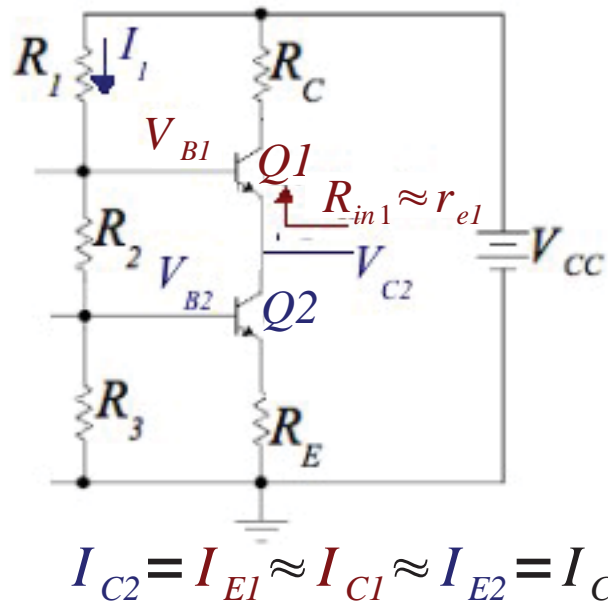
## Cascode Bias Summary

SPECIFIED:  $A_v$ ,  $V_{CC}$ ,  $V_{C1}$  (CB collector voltage);

SPECIFIED:  $I_E$  (or  $I_C$ ) directly or indirectly through  $BW$ .

DETERMINE:  $R_C$ ,  $R_E$ ,  $R_1$ ,  $R_2$  and  $R_3$ .

SET:  $V_{B1} - V_{B2} = 1V \Rightarrow V_{CE2} = 1V$



STEP1:  $R_C = \frac{V_{C1}}{I_C}$      $R_E = \frac{R_C}{|A_v|}$

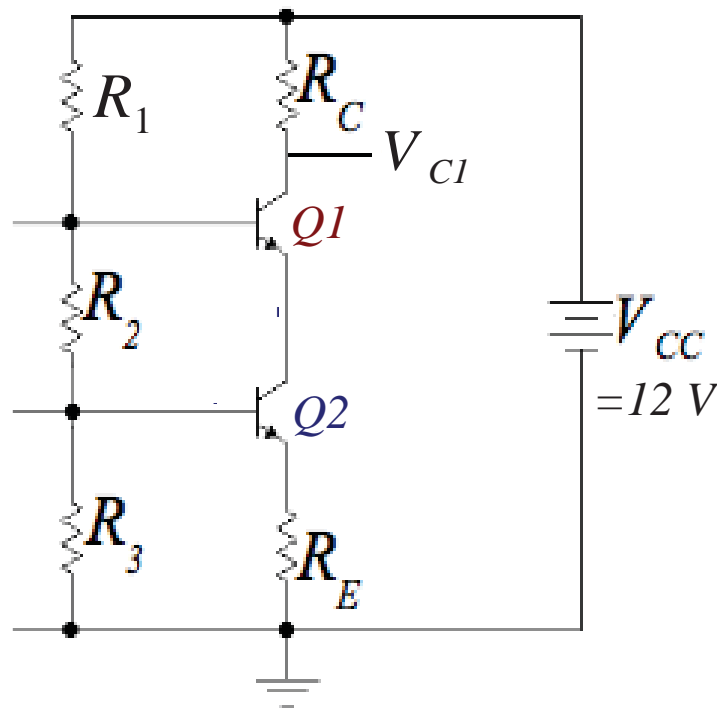
STEP2:  $R_2 = \frac{V_{B1} - V_{B2}}{I_1} = \frac{1V}{0.1 I_C}$

STEP3:  $R_3 = \frac{V_{B2}}{I_1} = \frac{0.7V + I_E R_E}{0.1 I_C}$

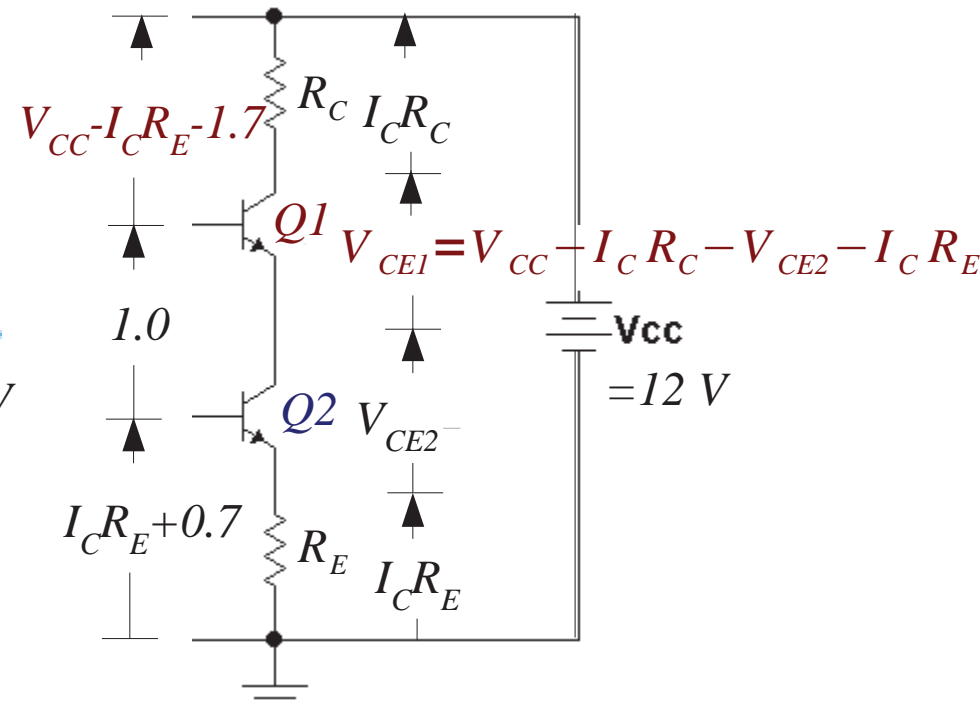
$$R_1 + R_2 + R_3 = \frac{V_{CC}}{I_1} = \frac{V_{CC}}{0.1 I_C}$$

STEP4:  $R_1 = \frac{V_{CC}}{0.1 I_C} - R_2 - R_3$

## Cascode Bias Example



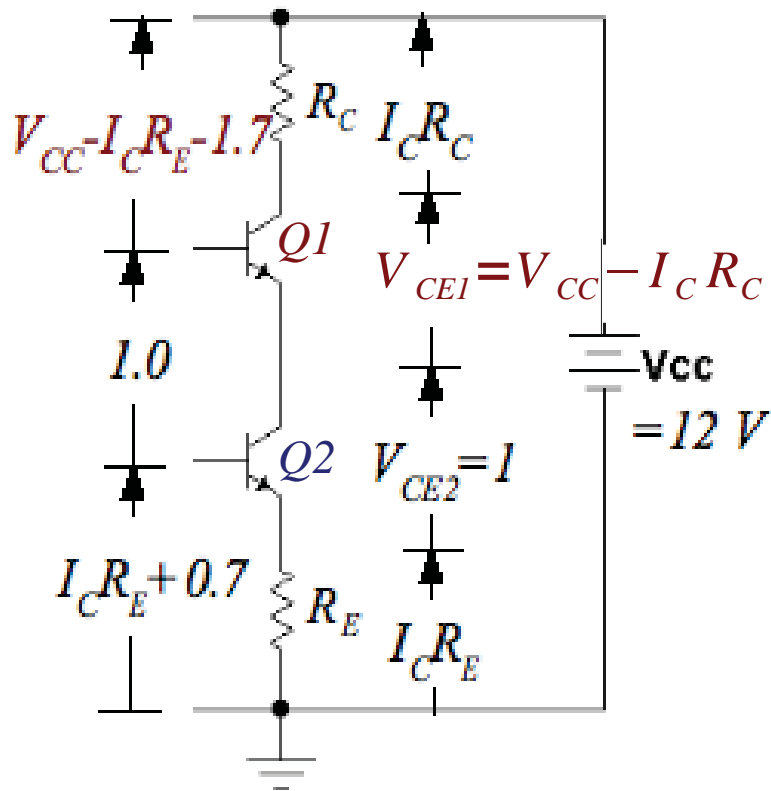
Cascode Amp



$$I_{E2} \approx I_{C2} = I_{E1} \approx I_{C1} \Rightarrow I_{C1} \approx I_{E2}$$

Typical Bias Conditions

## Cascode Bias Example cont.



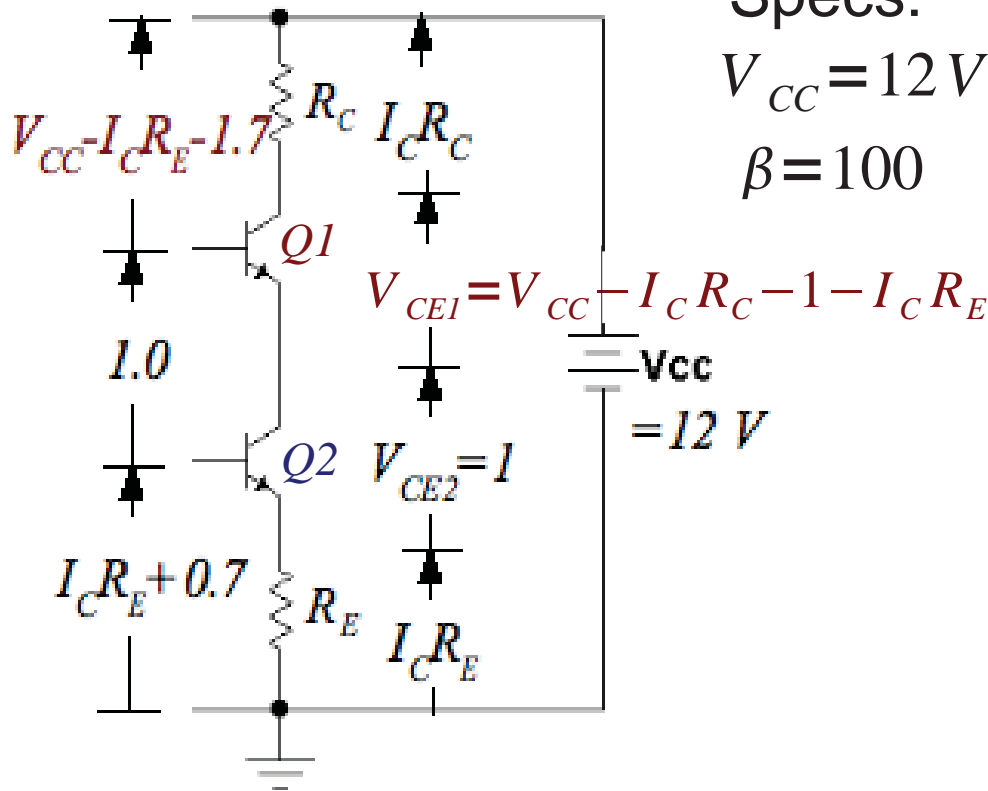
1. Choose  $I_{E1}$  – to set  $r_e$ .

Try  $I_{E1} = 5\text{ mA} \Rightarrow r_e = 0.025\text{ V} / I_E = 5\ \Omega$ .

2. Set desired gain magnitude. For example if  $A_V = -10$ , then  $R_C/R_E = 10$ .

3. Since the CE stage gain is very small,  $V_{CE2}$  can be small, i.e.  $V_{CE2} = V_{B1} - V_{B2} = 1\text{ V}$ .

## Cascode Bias Example cont.



Specs:

$$V_{CC} = 12V \quad V_{C1} = 7V \quad I_C = 5mA \quad |A_v| = \frac{R_C}{R_E} = 10$$

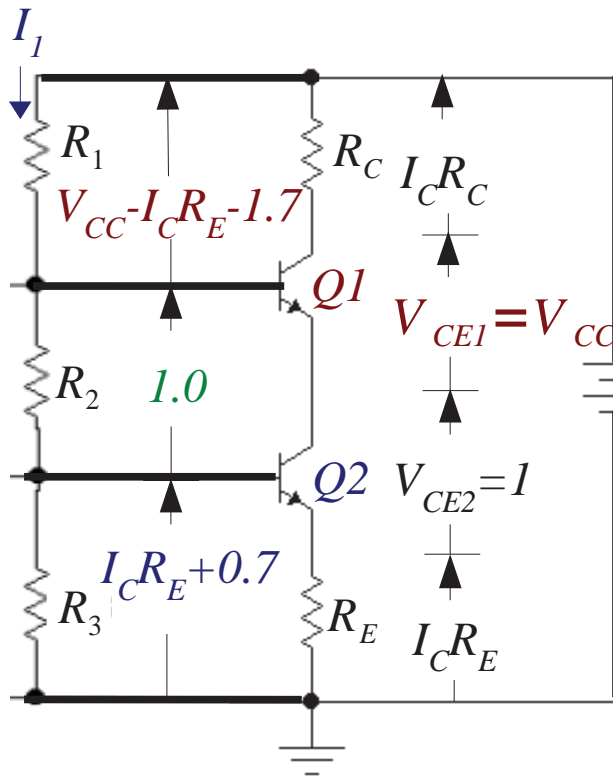
$$\beta = 100$$

Determine  $R_C$  for  $V_{C1} = 7V$ .

$$R_C = \frac{V_{CC} - V_{C1}}{I_C} = \frac{5V}{5 \cdot 10^{-3} A} = 1000 \Omega$$

$$R_E = \frac{R_C}{|A_v|} = \frac{R_C}{10} = 100 \Omega$$

## Cascode Bias Example cont.



$$V_{CC} = 12 \quad R_C = 1 \text{ k}\Omega \quad I_C = 5 \text{ mA} \quad R_E = 100 \Omega$$

Make current through the string of bias resistors  $I_1 = 0.1 I_C = 0.5 \text{ mA}$ .

$$R_1 + R_2 + R_3 = \frac{V_{CC}}{I_1} = \frac{12}{5 \cdot 10^{-4}} = 24 \text{ k}\Omega$$

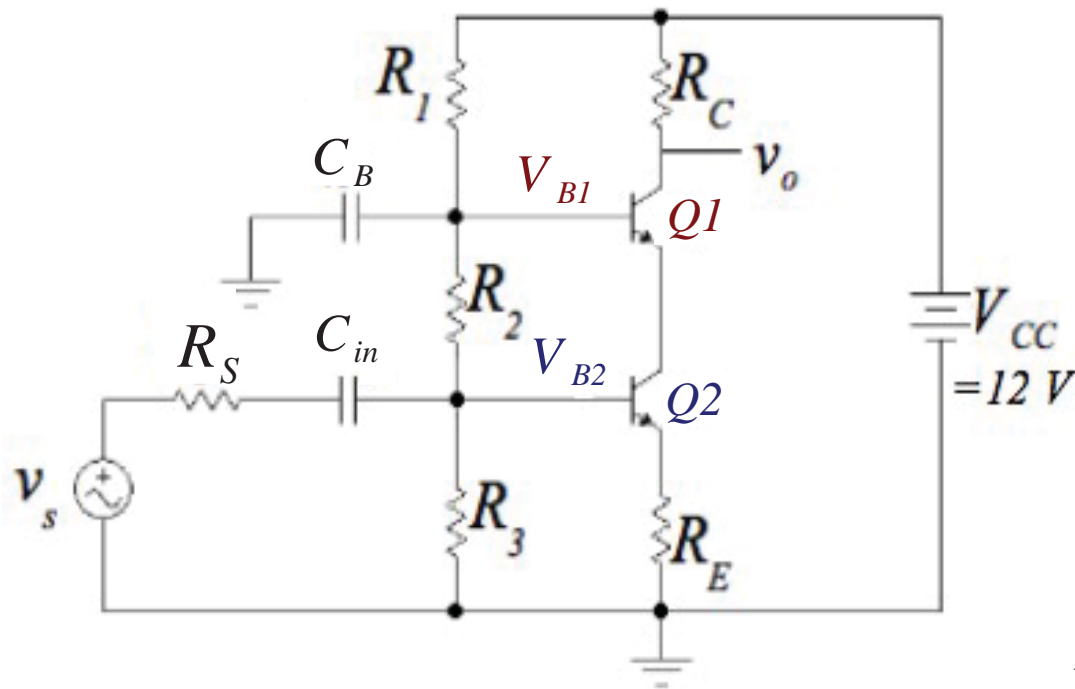
Calculate the bias voltages (base side of Q1, Q2):

$$V_{R1} = V_{CC} - I_C R_E - 1.7 \text{ V} = 12 \text{ V} - 0.5 \text{ V} - 1.7 \text{ V} = 9.8 \text{ V}$$

$$V_{R2} = V_{B1} - V_{B2} = 1 \text{ V}$$

$$V_{R3} = V_{B2} = I_C R_E + 0.7 = 5 \cdot 10^{-3} \cdot 100 + 0.7 = 1.2 \text{ V}$$

## Cascode Bias Example cont.



$$V_{B2} = 5 \cdot 10^{-4} R_3 = 1.2 \text{ V}$$

$$R_3 = 2.4 \text{ k} \Omega$$

$$V_{B1} - V_{B2} = 5 \cdot 10^{-4} R_2 = 1.0 \text{ V}$$

$$R_2 = 2 \text{ k} \Omega$$

$$\text{Recall: } R_1 + R_2 + R_3 = 24 \text{ k} \Omega$$

$$R_1 = 24000 - 2400 - 2000 = 19.6 \text{ k} \Omega$$

$$V_{CC} = 12, \quad R_C = 1 \text{ k} \Omega, \quad V_{B2} = 1.2 \text{ V},$$

$$I_C = 5 \text{ mA}, \quad R_E = 100 \Omega, \quad V_{B1} - V_{B2} = 1.0 \text{ V}$$

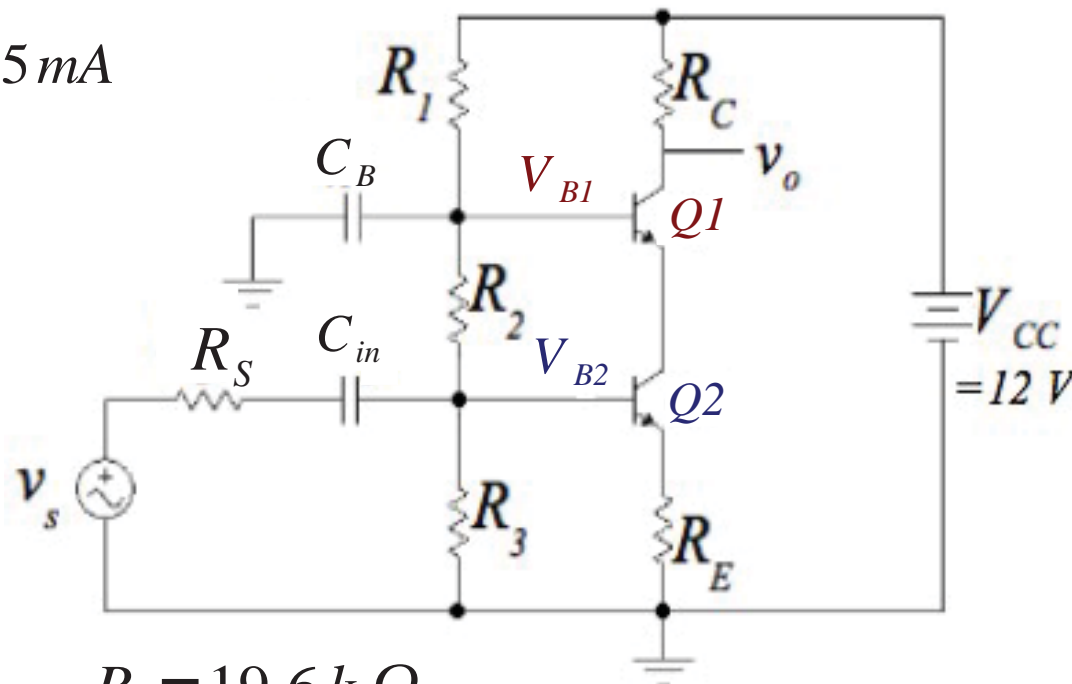
## Completed Design

$$\beta = 100$$

$$r_e = 5 \Omega \Rightarrow I_C = 5 \text{ mA}$$

$$V_{CE} = 7 \text{ V}$$

$$|A_v| = \frac{R_C}{R_E} = 10$$



$$R_1 = 19.6 \text{ k}\Omega$$

$$R_2 = 2 \text{ k}\Omega$$

$$R_3 = 2.4 \text{ k}\Omega$$

$$R_C = 1 \text{ k}\Omega$$

$$R_E = 100 \Omega$$

NOTE:  $R_B = R_2 \parallel R_3 = 1.09 \text{ k}\Omega \ll \beta R_E = 10 \text{ k}\Omega$

$$f_H = \frac{1}{2\pi C_{tot} R'_S}$$

$$C_{tot} = C_\pi + \left(1 + \frac{r_e}{R_E}\right) C_\mu$$

$$= C_\pi + 1.05 C_\mu$$

$$\text{If } C_\pi = 12 \text{ pF}$$

$$C_\mu = 2 \text{ pF}$$

$$C_{tot} = 14.1 \text{ pF}$$

$$f_{H\text{cascode}} = 225.8 \text{ MHz}$$

For CE with  $|A_v| = 10$

$$f_{HCE} = 94 \text{ MHz}$$